

## **C5.4 Pretensioned Prestressed Concrete Beam**

See the Office of Bridges and Structures web site for archived Methods Memos listed under articles in this section.

The Methods Memos for which policies have been partially revised and/or for which document references have been updated are noted as partially revised. Any obsolete Methods Memos that apply to this section are listed at the end.

### **C5.4.2 PPCB LRFD**

#### **C5.4.2.1 General**

##### **C5.4.2.1.1 Policy overview**

**Methods Memo No. 159: Policy on Bulb Tee Use**

**1 June 2008**

**Methods Memo No. 77: Changes to new BTC and BTB Beams (Supersedes Methods Memo No. 66 in cases of conflict)**

**14 January 2003**

**Methods Memo No. 84: New Beam Standard Development**

**24 July 2003**

**Methods Memo No. 73: Use of Special Prestressed Beam Designs**

**30 December 2004**

##### **C5.4.2.1.2 Design information**

##### **C5.4.2.1.3 Definitions**

##### **C5.4.2.1.4 Abbreviations and notation**

**Methods Memo No. 77: Changes to new BTC and BTB Beams (Supersedes Methods Memo No. 66 in cases of conflict)**

**14 January 2003**

**Methods Memo No. 84: New Beam Standard Development**

**24 July 2003**

##### **C5.4.2.1.5 References**

#### **C5.4.2.2 Loads**

##### **C5.4.2.2.1 Dead**

**Methods Memo No. 24: Beam Design and Bearing Design, Distribution of Dead Load 2**  
**4 September 2001 (Under LRFD this memo will apply to DC2 and DW loads.)**

##### **C5.4.2.2.2 Live**

**Methods Memo No. 182: LRFD Live Load Distribution for Skewed Bridges with Non-standard Rolled Steel Beams, Non-standard Prestressed Beams or Welded Plate Girders**

1 July 2008

**Methods Memo No. 40: Exterior Beam Distribution Factor -- LRFD**  
28 August 2001

#### **C5.4.2.2.3 Dynamic load allowance**

#### **C5.4.2.2.4 Earthquake**

#### **C5.4.2.2.5 Construction**

### **C5.4.2.3 Load application to superstructure**

#### **C5.4.2.3.1 Load modifier**

#### **C5.4.2.3.2 Limit states**

##### **Memo 5.4.2.3.2, 5.5.2.3.2, and 5.6.2.3.2-2011 ~ Strength V Limit State During Construction and Other Revisions**

Based on the description in the AASHTO LRFD Specifications of the Strength V limit state it seemed that it was not intended to be checked during construction. However, a steel plate girder example by M.A. Grubb and R.E. Schmidt distributed nationally by the U.S. Department of Transportation (USDOT) and National Steel Bridge Alliance (NSBA) includes Strength V during construction. The description of Strength V notes: "...plus 1.35 times the design live load (or any temporary live loads acting on the structure when evaluating the construction condition), plus 0.4 times the wind load on the structure, plus 1.0 times the wind on the live load. For evaluating the construction condition under the STRENGTH V load combination, the load factor for temporary dead loads that act on the structure during construction is not to be taken less than 1.25 and the load factor for any non-integral wearing surface and utility loads may be reduced from 1.5 to 1.25." Based on the example and other sources it is clear that Strength V should be checked during construction when appropriate, and articles in the design manual have been revised with respect to construction limit states. (There are several other changes, also.) The steel example is available at the following URL:

<http://www.virginiadot.org/business/resources/SteelDesignExample.pdf>

### **C5.4.2.4 A-D and BTB-BTE beams**

#### **C5.4.2.4.1 Analysis and design**

##### **C5.4.2.4.1.1 Analysis assumptions**

##### **C5.4.2.4.1.2 Materials**

**Methods Memo No. 80: Maximum Release and Final Concrete Strength for PPCB**  
15 April 2003

##### **C5.4.2.4.1.3 Design resistance and stress limits**

##### **C5.4.2.4.1.4 Section properties**

**Methods Memo No. 97: Revision of MM No. 83 Camber Calculations Using Transformed Sections for Prestressed Beam Design**  
21 May 2004

**C5.4.2.4.1.5 Deflected strands****C5.4.2.4.1.6 Prestress losses****C5.4.2.4.1.7 Moment**

15 March 2012

In the past the Iowa DOT has designed PPCB superstructures by designing the beams for simple spans and detailing for continuity but then also checking the beams in the continuous condition. Generally the beams and deck were adequate for all continuity checks near and at a pier. With development of longer beams, however, service checks at the transfer points and compression checks for negative moment at continuity diaphragms began to fail under some conditions. It also was difficult to place enough tension reinforcement in the deck. As a result the office has decided not to check the continuous condition for concrete compression, taking full advantage of the exception for simple spans in the AASHTO LRFD Specifications [AASHTO-LRFD 5.14.1.4.1].

In order to avoid construction difficulties the office is limiting the reinforcing in the deck so that longitudinal bar spacing is not too close and bars are not too large. In unusual cases these limitations may result in less reinforcement in the deck than would be required for the negative moment at the strength limit state. The office is willing to accept that condition on a case-by-case basis and intends to monitor field performance.

The continuity condition above a pier during service is difficult to determine accurately. Under typical Iowa DOT procedures and specifications the designer has minimal control over the age of beams at the time the pier diaphragm and deck are poured. Effects of creep and shrinkage after the superstructure is continuous also are difficult to quantify even when the age of beams is known. Generally creep and shrinkage effects are relieved at ultimate conditions by concrete cracking and mild reinforcement yielding, and therefore the office considers the exceptions noted above to be reasonable, and the exceptions are permissible under the AASHTO LRFD Specifications.

**C5.4.2.4.1.8 Shear****C5.4.2.4.1.9 Deflection and camber****C5.4.2.4.1.10 Anchorage zone****C5.4.2.4.1.11 Handling and shipping****C5.4.2.4.1.12 Additional considerations****C5.4.2.4.2 Detailing**

Methods Memo No. 99: Update of Bid Item Codes for BTC and BTB  
16 July 2004

Methods Memo No. 73: Use of Special Prestressed Beam Designs  
30 December 2004

Methods Memo No. 105: Use of Epoxy-Coated Reinforcing Steel  
28 March 2005

Methods Memo No. 56: Sealing of PCBM Ends  
22 October 2003

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**Obsolete: Methods Memo No. 36: Miscellaneous Design and Detailing Issues for 71½ (1800 mm) Bulb Tee**  
7 January 2002

**Obsolete: Methods Memo No. 66: Guidelines for Using Standard Prestressed Concrete Beams**  
27 August 2002 (Much of this memo was superseded by MM No. 77 on 14 January 2003.)

**Obsolete: Methods Memo No. 83: Camber Calculations Using Transformed Sections**  
11 April 2003 (This memo was superseded by Methods Memo No. 97 on 21 May 2004.)

**Obsolete: Methods Memo No. 106: End Beam Dimension for BTC**  
7 February 2005

**Obsolete: Methods Memo No. 147: Embedded Deck Hanger Forms in PPCB**  
15 May 2007 (This memo was superseded by MM No. 197, 1 May 2008.)

**Obsolete: Methods Memo No. 183: Policy Regarding Construction Loading**  
1 January 2008

**Obsolete: Methods Memo No. 197: Revision to E/M 202 – Embedded Deck Hangers in PPCB**  
1 May 2008